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Frequency doubling in Cavity-Resonator Integrated Grating Filter

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ABSTRACT

Guided Mode Resonant Filters (GMRFs) have long been studied as a support surface for nonlinear optical interactions due to their intrinsically high Q-factor. However, their operation relies on a non-localized and large-area guided mode that limits the achievable power density and requires complex phase-matching approaches. Conversely, photonic crystal nano-cavities have shown promising results due to both their high-Q factors to enhance the pump field and their localized nature that allows phase-matching-free implementation and high power density excitation. However, their intrinsic small size restricts the supported input power and hinders the coupling efficiency of the pump into the mode.

In this paper, we report the first experimental demonstration of continuous-wave second harmonic generation in a Cavity-Resonator Integrated Grating Filter (CRIGF). This intermediary device, which can be described as a cavity-enhanced finite-size GMRF or, equivalently, as a low-index-contrast photonic crystal micro-cavity, will be shown to offer a practical route to nonlinear interactions with viable power (<20 mW) and excitation conditions (surface excitation with a ~10- μ m-waist spot size). In practice, the devices under study make use of a lithium-niobate on insulator (LNOI) waveguide with a nanostructured silicon nitride upper cladding as a pragmatic way to implement a high second-order nonlinearity platform with established processing technology. The already-demonstrated versatility of the CRIGF design (demonstrated at wavelengths of 850 nm using S₃iN₄/SiO₂ platform, 4.5 μ m with the GaAs/AlGaAs technology and, here, at 1.55 μ m with the LiNbO₃ platform) coupled to the electro-optical tuning afforded by lithium niobate system makes this approach extremely promising for pixelated non-linear systems.

Keywords: second harmonic generation, guided-mode resonance filters, lithium niobate, cavity-resonant integrated grating filter, nonlinear frequency conversion

1. INTRODUCTION

Guided Mode Resonant Filters (GMRFs) have been studied as devices for nonlinear optical interactions due to their intrinsically high Q-factor^{1,2}. Given that their principle is based on non-localized and large-area guided mode(s), to ensure an efficient nonlinear conversion, the excitation beam needs to have a low-divergence and be wide and thereby the operation is inherently limited by the achievable power density. Furthermore, to achieve the constructive harmonic generation over such large surfaces, the phase-matching condition has to be strictly met. Conversely, photonic crystal nano-cavities have shown promising results due to both their high-Q factors to enhance the pump field and their localized nature that allows phase-matching-free implementation and high power density excitation^{3,4}. However, their intrinsic small size restricts the supported input power and hinders the coupling efficiency of the pump into the mode.

In this paper, we report the first experimental demonstration of continuous-wave second harmonic generation (SHG) in a low-index-contrast photonic crystal micro-cavity or equivalently in cavity-enhanced finite-size GMRF that is also known as a Cavity-Resonant Integrated Grating Filter (CRIGF)^{5,6}. Practically, the device was made using a hybrid lithium niobate and silicon-oxynitride technology.

2. DESIGN

As shown on Figure 1, the considered CRIGF structure relies on a lithium-niobate-on-insulator (LNOI) substrate since this technological platform combines a high non-linear susceptibility (of 33pm/V) with an ability to make high-confinement but low-loss waveguides⁷⁻⁹. Here, the sample consists of a 297-nm-thick X-cut lithium-niobate core on a 2 μ m-thick SiO₂-coated lithium-niobate substrate of similar orientation.

We chose to use two additional layers (made of Si₃N₄ and SiO₂) to form the upper-cladding of the waveguide such that we could create an anti-reflective multilayer stack at the fundamental wavelength of design (1555 nm) under surface-normal excitation and choose the bandwidth of the Distributed Bragg Reflectors that sets the micro-cavity. From these thicknesses, we defined the coupling grating and DBR constitutive parameters based on standard effective index calculation of the TE-polarized mode and set the phase section length to obtain a resonance at the design wavelength. The resulting parameters are listed in Table 1 and Figure 1. Further details on the design procedure can be found in¹⁰.

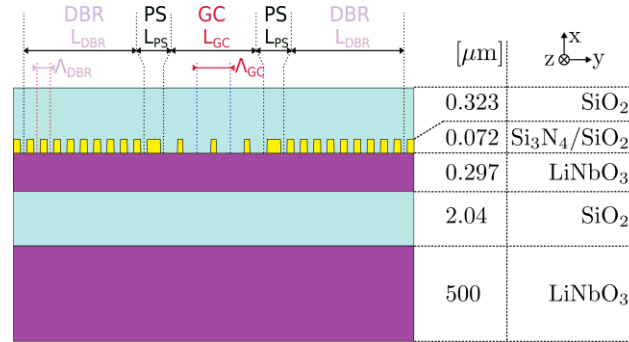


Figure 1. Schematic of the CRIGF structure under study

Table 1. Parameters of the CRIGF nano-structured elements.

Parameter	Value
Grating coupler period (nm)	865
Grating coupler number of periods	10.5
Grating coupler fill factor	0.45
DBR period (nm)	432
DBR number of periods	400
DBR fill factor	0.5
Phase section length (nm)	973

Using RCWA calculations and assuming a mode-matched excitation and a loss-less waveguide, the CRIGF is shown to have a ~ 1 nm bandwidth with a maximum reflectivity of 85.3% and minimum transmission of 14.7% (see Figure 2). The generated second harmonic signal was also calculated under the undepleted pump approximation and is shown on Figure 2 to be exalted at the device resonance. Further information on the calculations are available in reference ¹¹ together with a comparison to the expected results from substrate-only and GMRF-based generation.

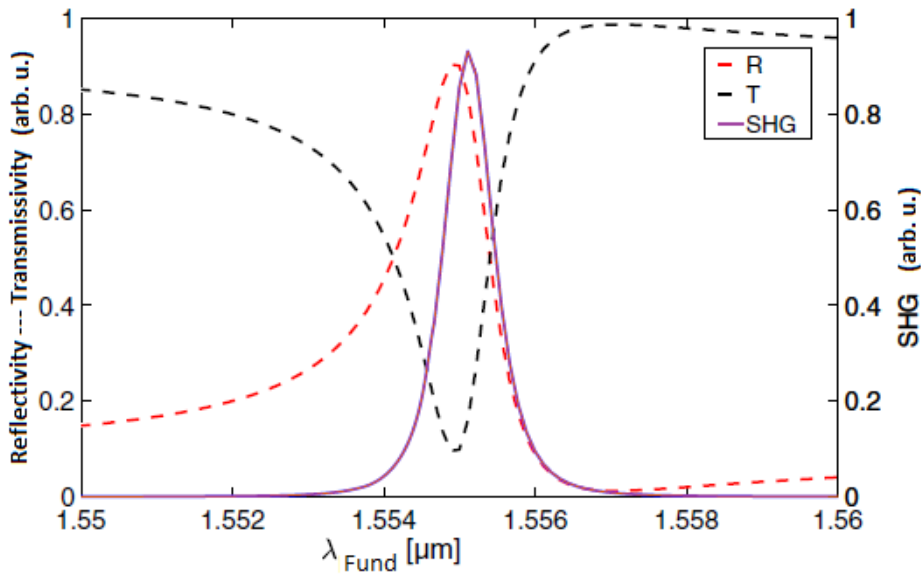


Figure 2. Calculated spectral reflectivity (black) and transmission (grey) of the designed CRIGF.

To complement this information, we also computed the substrate-radiating SHG pattern presented in Figure 3 by selecting the modal content whose wavevectors are above the light cone. The SHG emission diagram exhibits three peaks that can be assigned to the extraction of the SHG signal by the grating-coupler section (through the 0th and $\pm 1^{\text{st}}$ orders).

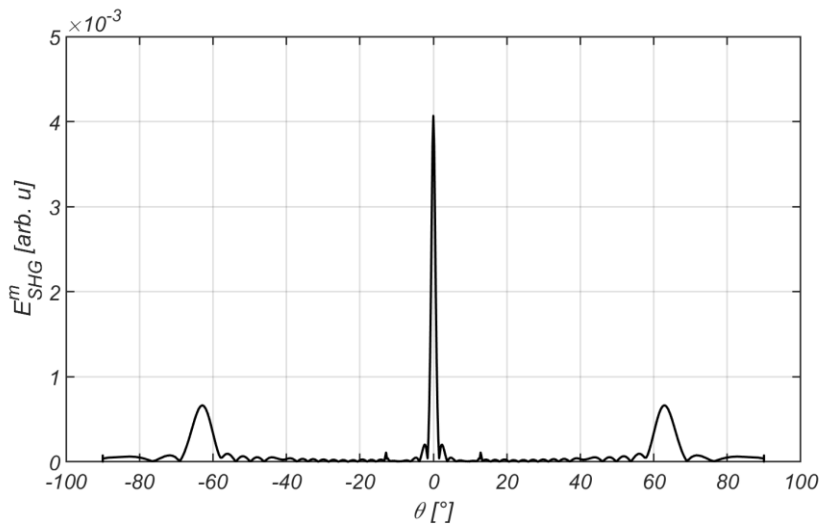


Figure 3. Radiation pattern in air of the second harmonic signal for the considered CRIGF.

3. FABRICATION

The device fabrication started from the LNOI planar waveguide described above obtained from NanoLN. The first layer of the waveguide upper-cladding layer, made of Si_3N_4 , was deposited using an Inductive-Coupled-Plasma Plasma-Enhanced Chemical Vapor Deposition system. The designed gratings were subsequently patterned into this layer using nano-imprint lithography¹² and dry etching with the LiNbO_3 top surface acting as an etch-stop interface. The device fabrication was completed by the deposition of a 323-nm-thick SiO_2 upper cladding layer on top of the grating structure and of a 266-nm-thick SiO_2 single-layer anti-reflective coating on the rear-side of the substrate to avoid back-reflection.

4. CHARACTERISATION

The sample was characterized using the setup shown in Figure 4. The tunable source delivered up to 17 mW of fundamental signal at a wavelength tunable from 1500 to 1630 nm with a linewidth of ~ 100 kHz and was optically relayed using a telescope system to ensure mode-matched excitation of the CRIGF. The generated second harmonic signal was collected using a NA=0.15 lens, separated from the pump using a dichroic filter and analyzed using a visible spectrum analyzer. In the absence of an InGaAs camera, the 980nm beam served as a guide to align the 1550 nm beam and was turned off during the measurements.

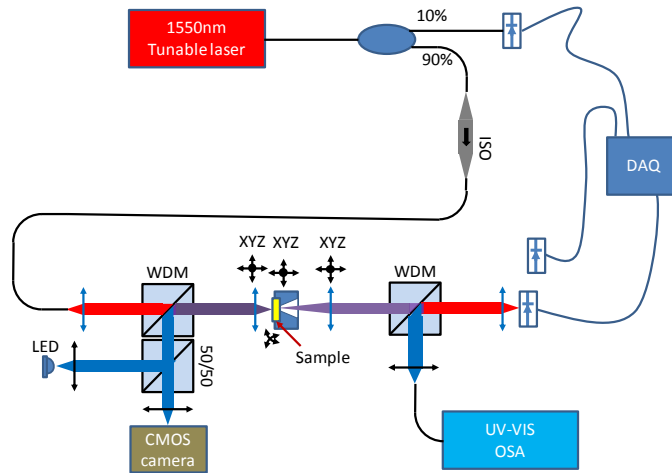


Figure 4. Setup used for that characterisation of the considered CRIGF.

As shown in Figure 5, the second harmonic signal is observed to increase significantly at a wavelength of 1555 nm corresponding to the device resonance. We were also able to establish that a fraction of the SHG signal is also diffracted at $\sim \pm 60^\circ$, in agreement with the above-displayed calculated radiation pattern.

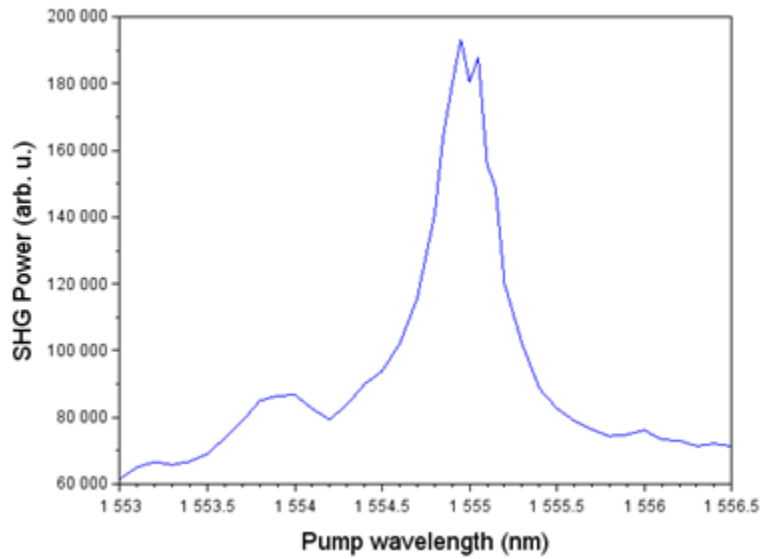


Figure 5. CRIGF SHG spectral characteristic recorded at normal incidence.

Polarization analysis reveals that the second harmonic emission is TE-polarized as expected and accounted for in the numerical simulations.

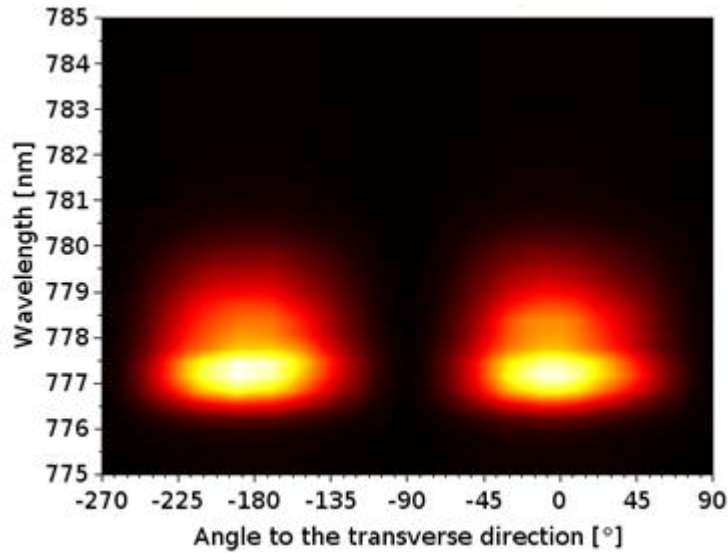


Figure 6. Measurement of the SHG polarisation state ($\alpha=0^\circ$ for analysis polarizer along the grating lines).

Finally, the measurement of the performance on three devices with scaled designs (corresponding grating coupler periods of 845, 865 and 885 nm) enabled to demonstrate the linear dependence of the SHG wavelength to the device design parameter (or equivalently resonant wavelength), consistent with cavity-enhanced SHG operation.

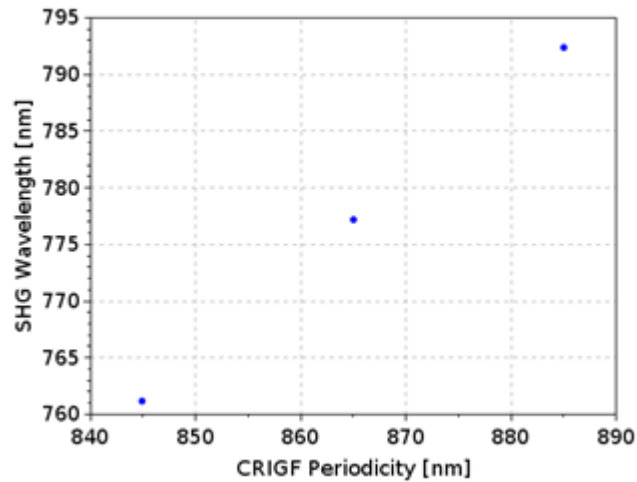


Figure 7. SHG tunability with CRIGF design parameter (here taken to be the grating coupler period).

5. CONCLUSION

We demonstrated successful continuous-wave SHG enhancement in CRIGF structures made using a hybrid lithium-niobate/silicon oxynitride technology. Future prospects will be to look for improved nonlinear conversion performance using a combination of optimised SHG-CRIGF designs and improved fabrication processes.

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